## Step-up DC / DC Converter with Overcurrent Protection

NO.EA-272-230928

## OUTLINE

The R1205x is a PWM control type step-up DC/DC converter IC with low supply current. Each of these ICs consists of an NMOS FET, a diode, an oscillator, a PWM comparator, a voltage reference unit, an error amplifier, a current limit circuit, an under voltage lockout circuit (UVLO), an over-voltage protection circuit (OVP), a softstart circuit, a Maxduty limit circuit, and a thermal shutdown protection circuit. This step-up DC/DC converter can be easily built with a few external components such as a coil, a resistor, and a capacitor. As the protection functions, the R1205x has an Lx peak current limit function, an over voltage protection (OVP) function, an under voltage lock out (UVLO) function and a thermal shutdown function.
The R1205x presents the R1205x8xxA version that is optimized for the constant voltage power source, and the R1205x8xxB/C version that is optimized for driving the white LED with the constant current. The R1205x8xxB/C is an adjustable version that can change the LED brightness dynamically by using a 200 Hz to 300 kHz PWM signal toward the CE pin.
The R1205x is available in DFN1616-6B and TSOT-23-6 packages.

## FEATURES

- Input Voltage Range
2.3 V to 5.5 V (R1205x8xxA)
1.8 V to 5.5 V (R1205x8xxB/C)
- Supply Current Typ. $800 \mu \mathrm{~A}$
- Standby Current Max. $5 \mu \mathrm{~A}$
- Feedback Voltage $1.0 \mathrm{~V} \pm 15 \mathrm{mV}$ (R1205x8xxA) $0.2 \mathrm{~V} \pm 10 \mathrm{mV}(\mathrm{R} 1205 \mathrm{x} 8 \mathrm{xxB})$ $0.4 \mathrm{~V} \pm 10 \mathrm{mV}$ (R1205x8xxC)
- Oscillator Frequency

Typ. 1.2MHz

- Maximum Duty Cycle Typ. 91\%
- UVLO Function

Typ.2.0V (Hys.Typ.0.2V) (R1205x8xxA)
Typ.1.6V (Hys.Typ.0.1V) (R1205x8xxB/C)

- Selectable Lx Current Limit Function.................... Typ. 350mA / 700mA
- Over Voltage Protection

Typ. 25V

- LED dimming control (R1205x8xxB/C) ...............by external PWM signal (Frequency 200Hz to 300kHz)
- Thermal Protection Function

Typ. $150^{\circ} \mathrm{C}$ (Hys.Typ. $50^{\circ} \mathrm{C}$ )

- Switch ON Resistance

Typ. 1.35

- Packages

DFN1616-6B, TSOT-23-6

- Ceramic capacitors are recommended


## APPLICATION

- Constant Voltage Power Source for portable equipment
- OLED power supply for portable equipment
- White LED Backlight for portable equipment


## SELECTION GUIDE

The OVP threshold voltage, current limit, package and $V_{F B} /$ Auto discharge are user-selectable options.

| Product Name | Package | Quantity per Reel | Pb Free | Halogen Free |
| :--- | :---: | :---: | :---: | :---: |
| R1205L8x1*-TR | DFN1616-6B | 5,000 pcs | Yes | Yes |
| R1205N8x3*-TR-FE | TSOT-23-6 | $3,000 \mathrm{pcs}$ | Yes | Yes |

$x$ : Designation of current limit.
(1) 350 mA
(2) 700 mA

* : Designation of VFB.
(A) 1.0 V
(B) 0.2 V
(C) 0.4 V


## BLOCK DIAGRAMS



## PIN DESCRIPTIONS

DFN1616-6B

## Top View



Bottom View


TSOT-23-6


DFN1616-6B

| Pin No | Symbol | Pin Description |
| :---: | :---: | :--- |
| 1 | CE | Chip Enable Pin ("H" Active) |
| 2 | VFB | Feedback Pin |
| 3 | LX | Switching Pin (Open Drain Output) |
| 4 | GND | Ground Pin |
| 5 | VIN | Input Pin |
| 6 | VOUT | Output Pin |

* The tab is substrate level (GND). The tab is better to be connected to the GND, but leaving it open is also acceptable.

TSOT-23-6

| Pin No | Symbol | Pin Description |
| :---: | :---: | :--- |
| 1 | CE | Chip Enable Pin ("H" Active) |
| 2 | VOUT | Output Pin |
| 3 | VIN | Input Pin |
| 4 | LX | Switching Pin (Open Drain Output) |
| 5 | GND | Ground Pin |
| 6 | VFB | Feedback Pin |

# ABSOLUTE MAXIMUM RATINGS 

GND=0V

| Symbol |  | Item | Rating | Unit |
| :---: | :---: | :---: | :---: | :---: |
| Vin | VIN Pin Voltage |  | -0.3 to 6.5 | V |
| Vce | CE Pin Voltage |  | -0.3 to 6.5 | V |
| $V_{\text {FB }}$ | VFB Pin Voltage |  | -0.3 to 6.5 | V |
| Vout | VOUT Pin Voltage |  | -0.3 to 28 | V |
| VLx | LX Pin Voltage |  | -0.3 to 28 | V |
| ILx | LX Pin Current |  | 1000 | mA |
| PD | Power Dissipation ${ }^{(1)}$ | DFN1616-6B <br> (JEDEC STD. 51-7 Test Land Pattern) | 2400 | mW |
|  |  | TSOT-23-6 <br> (Standard Test Land Pattern) | 460 |  |
| Tj | Junction Temperature Range |  | -40 to 125 | ${ }^{\circ} \mathrm{C}$ |
| Tstg | Storage Temperature Range |  | -55 to 125 | ${ }^{\circ} \mathrm{C}$ |

## ABSOLUTE MAXIMUM RATINGS

Electronic and mechanical stress momentarily exceeded absolute maximum ratings may cause permanent damage and may degrade the life time and safety for both device and system using the device in the field.
The functional operation at or over these absolute maximum ratings are not assured.

## RECOMMENDED OPERATING CONDITIONS

| Symbol | Item | Rating | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\mathrm{IN}}$ | Input Voltage (R1205x8xxA) | 2.3 to 5.5 | V |
|  | Input Voltage (R1205x8xxB/C) | 1.8 to 5.5 |  |
| Ta | Operating Temperature Range | -40 to 85 | ${ }^{\circ} \mathrm{C}$ |

## RECOMMENDED OPERATING CONDITIONS

All of electronic equipment should be designed that the mounted semiconductor devices operate within the recommended operating conditions. The semiconductor devices cannot operate normally over the recommended operating conditions, even if they are used over such ratings by momentary electronic noise or surge. And the semiconductor devices may receive serious damage when they continue to operate over the recommended operating conditions.
${ }^{(1)}$ Refer to POWER DISSIPATION for detailed information.

## ELECTRICAL CHARACTERISTICS

R1205x
( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )

| Symbol | Item | Conditions |  | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ido | Supply Current | $\mathrm{V}_{\mathrm{IN}}=5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=0 \mathrm{~V}$, Lx at no load |  |  | 0.8 | 1.2 | mA |
| Istandby | Standby Current | $\mathrm{V}_{\text {IN }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=0 \mathrm{~V}$ |  |  | 1.0 | 5.0 | $\mu \mathrm{A}$ |
| Vuvlo 1 | UVLO Detector Threshold | VIN falling | R1205x8xxA | 1.9 | 2.0 | 2.1 | V |
|  |  |  | R1205x8xxB/C | 1.5 | 1.6 | 1.7 |  |
| Vuvloz | UVLO Released Voltage | VIN rising | R1205x8xxA |  | $\begin{gathered} \text { VuvLO1 } \\ +0.2 \end{gathered}$ | 2.3 | V |
|  |  |  | R1205x8xxB/C |  | Vuvlo1 $+0.1$ | 1.8 |  |
| Vceh | CE Input Voltage "H" | $\mathrm{V}_{\mathrm{IN}}=5.5 \mathrm{~V}$ |  | 1.5 |  |  | V |
| Vcel | CE Input Voltage "L" |  |  |  |  | 0.5 | V |
| Rce | CE Pull Down Resistance |  |  |  | 1200 |  | $k \Omega$ |
| $V_{\text {fb }}$ | V ${ }_{\text {fb }}$ Voltage Accuracy | $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$ | R1205x8xxA | 0.985 | 1.000 | 1.015 | V |
|  |  |  | R1205x8xxB | 0.19 | 0.2 | 0.21 |  |
|  |  |  | R1205x8xxC | 0.39 | 0.4 | 0.41 |  |
| $\begin{gathered} \Delta \mathrm{V}_{\mathrm{FB}} / \\ \Delta \mathrm{Ta} \end{gathered}$ | $V_{\text {FB }}$ Voltage Temperature Coefficient | $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V},-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 85^{\circ} \mathrm{C}$ |  |  | $\pm 150$ |  | $\underset{/^{\circ} \mathrm{C} \mathrm{C}}{\mathrm{ppm}}$ |
| Ifb | VFb Input Current | $\mathrm{V}_{\mathrm{IN}}=5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=0 \mathrm{~V}$ or 5.5 V |  | -0.1 |  | 0.1 | $\mu \mathrm{A}$ |
| tstart | Soft-start Time |  | R1205x8xxA |  | 2.0 | 3.0 | ms |
| Ron | FET ON Resistance | l Lx $=100 \mathrm{~mA}$ |  |  | 1.35 |  | $\Omega$ |
| loff | FET Leakage Current | V Lx $=24 \mathrm{~V}$ |  |  |  | 3.0 | $\mu \mathrm{A}$ |
| ILım | FET Current Limit |  | R1205x81xx | 250 | 350 | 450 | mA |
|  |  |  | R1205x82xx | 500 | 700 | 900 |  |
| $V_{F}$ | Diode Forward Voltage | Isw $=100 \mathrm{~mA}$ |  |  | 0.8 |  | V |
| $\underline{\text { Idiodeleak }}$ | Diode Leakage Current | Vout $=24 \mathrm{~V}$, $\mathrm{V}_{\text {Lx }}=0 \mathrm{~V}$ |  |  |  | 10 | $\mu \mathrm{A}$ |
| fosc | Oscillator Frequency | $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\text {Fb }}=0 \mathrm{~V}$ |  | 1000 | 1200 | 1400 | kHz |
| Maxduty | Maximum Duty Cycle | $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}, \mathrm{~V}_{\text {FB }}=0 \mathrm{~V}$ |  | 86 | 91 |  | \% |
| Vovp1 | OVP Detect Voltage | $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}$ rising |  | 24.2 | 25 | 25.8 | V |
| Vovp2 | OVP Release Voltage | $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, Vout falling |  |  | $\begin{aligned} & \hline \text { Vovp1 } \\ & -1.8 \end{aligned}$ |  | V |
| Ttsd | Thermal Shutdown Detect Temperature | $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$ |  |  | 150 |  | ${ }^{\circ} \mathrm{C}$ |
| TTSR | Thermal Shutdown Release Temperature | $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$ |  |  | 100 |  | ${ }^{\circ} \mathrm{C}$ |

## THEORY OF OPERATION

## Operation of Step-Up DC/DC Converter and Output Current

<Basic Circuit>


## <Current through L>



There are two operation modes of the step-up PWM control-DC/DC converter. That is the continuous mode and discontinuous mode by the continuousness inductor.
When the transistor turns ON, the voltage of inductor $L$ becomes equal to Vin voltage. The increase value of inductor current (i1) will be

$$
\Delta \mathrm{i} 1=\mathrm{V}_{\mathrm{IN}} \times \operatorname{ton} / \mathrm{L}
$$

$\qquad$

As the step-up circuit, during the OFF time (when the transistor turns OFF) the voltage is continually supply from the power supply. The decrease value of inductor current (i2) will be

$$
\Delta i 2=\left(\text { Vout }-V_{\text {IN }}\right) \times \text { topen } / L
$$

At the PWM control-method, the inductor current become continuously when topen=toff, the DC/DC converter operate as the continuous mode.

In the continuous mode, the variation of current of i1 and i2 is same at regular condition.

$$
\text { Vin } \times \text { ton / L = (Vout - Vin }) \times \text { toff / L ................................................................................... Formula } 3
$$

The duty at continuous mode will be

$$
\text { duty }(\%)=\text { ton } /(\text { ton }+ \text { toff })=(\text { Vout - Vin }) / \text { Vout ................................................................. Formula } 4
$$

The average of inductor current at $\mathrm{tf}=$ toff will be

$$
\begin{aligned}
& \mathrm{IL}(\text { Ave. })=\mathrm{V}_{\mathrm{IN}} \times \operatorname{ton} /(2 \times \mathrm{L}) \\
& \text { Formula } 5
\end{aligned}
$$

If the input voltage = output voltage, the lout will be

If the lout value is large than above the calculated value (Formula 6), it will become the continuous mode, at this status, the peak current (ILmax) of inductor will be

$$
\begin{aligned}
& \text { ILmax }=\text { lout } \times \text { Vout } / \text { VIN }+ \text { VIN } \times \text { ton } /(2 \times \mathrm{L}) \\
& \text { ILmax }=\text { lout } \times \text { Vout }^{\prime} / \mathrm{V}_{\text {IN }}+\mathrm{V}_{\text {IN }} \times \mathrm{T} \times\left(\text { Vout }-\mathrm{V}_{\text {IN }}\right) /\left(2 \times \mathrm{L} \times \mathrm{V}_{\text {out }}\right)
\end{aligned}
$$

The peak current value is larger than the lout value. In case of this, selecting the condition of the input and the output and the external components by considering of ILmax value.
The explanation above is based on the ideal calculation, and the loss caused by Lxswitch and the external components are not included.
The actual maximum output current will be between $50 \%$ and $80 \%$ by the above calculations. Especially, when the IL is large or $\mathrm{V}_{\mathrm{IN}}$ is low, the loss of $\mathrm{V}_{\mathrm{IN}}$ is generated with on resistance of the switch. Moreover, it is necessary to consider Vf of the diode (approximately 0.8 V ) about Vout.

## Soft-Start (R1205x8xxA)

The output and referrence of the error amplifier start from 0 V and the referrence gradually rises up to 1.0 V . After the softstart time (TSS), output voltage rise up to the setting voltage.
The output of the error amplifier starts from 0 V and the inrush current is suppressed when starting by the CE pin "H" input. Moreover, the inrush current can be suppressed by gradually enlarging Duty of the PWM signal to the CE pin.

## Current Limit Function

Current limit function monitors the over current and if it reaches the peak current, it will turn off the driver. When the over current decreases, it will restart oscillation and will restart the monitoring.

## APPLICATION INFORMATION

## Typical Applications

R1205x8xxA


R1205x8xxB/C
L1


## Inductor Selection

The peak current of the inductor at normal mode can be estimated as the next formula when the efficiency is 80\%.

$$
\text { ILmax }=1.25 \times \text { lout } \times \text { Vout } / \mathrm{V}_{\text {IN }}+0.5 \times \mathrm{V}_{\text {IN }} \times\left(\mathrm{V}_{\text {out }}-\mathrm{VIN}_{\text {IN }}\right) /\left(\mathrm{L} \times \mathrm{V}_{\text {out }} \times \text { fosc }\right)
$$

In the case of start-up or dimming control by CE pin, inductor transient current flows, and the peak current of it must be equal or less than the current limit of the IC. The peak current should not beyond the rated current of the inductor.
The recommended inductance value is $10 \mu \mathrm{H}-22 \mu \mathrm{H}$.
Table 1 Peak current value in each condition

| Condition |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {IN }}(\mathrm{V})$ | Vout $(\mathrm{V})$ | Iout $(\mathrm{mA})$ | $\mathrm{L}(\mu \mathrm{H})$ | ILmax (mA) |
| 3 | 14 | 20 | 10 | 215 |
| 3 | 14 | 20 | 22 | 160 |
| 3 | 21 | 20 | 10 | 280 |
| 3 | 21 | 20 | 22 | 225 |

Table 2 Recommended inductors

| L <br> $(\mu \mathrm{H})$ | Part No. | Rated <br> Current $(\mathrm{mA})$ | Size <br> $(\mathrm{mm})$ |
| :---: | :---: | :---: | :---: |
| 10 | LQH32CN100K53 | 450 | $3.2 \times 2.5 \times 1.55$ |
| 10 | LQH2MC100K02 | 225 | $2.0 \times 1.6 \times 0.9$ |
| 10 | VLF3010A-100 | 490 | $2.8 \times 2.6 \times 0.9$ |
| 10 | VLS252010-100 | 520 | $2.5 \times 2.0 \times 1.0$ |
| 22 | LQH32CN220K53 | 250 | $3.2 \times 2.5 \times 1.55$ |
| 22 | LQH2MC220K02 | 185 | $2.0 \times 1.6 \times 0.9$ |
| 22 | VLF3010A-220 | 330 | $2.8 \times 2.6 \times 0.9$ |

## Capacitor Selection

Set $1 \mu \mathrm{~F}$ or more value bypass capacitor C 1 between V IN pin and GND pin as close as possible.

## R1205xxxxA

Set $1 \mu \mathrm{~F}-4.7 \mu \mathrm{~F}$ or more capacitor C 2 between Vout and GND pin.

Table 3-A Recommended components for R1205xxxxA

|  | Rated voltage(V) | Part No. |
| :---: | :---: | :---: |
| C1 | 6.3 | CM105B105K06 |
| C2 | 25 | GRM21BR11E105K |
| C3 | 25 | 22pF |
| R1 |  | For Vout Setting |
| R2 |  | For Vout Setting |
| R3 |  | $2 \mathrm{k} \Omega$ |

If the transient drop of output voltage by the load fluctuation is large and exceeds the allowable range in above setting, refer to Table 3-B to change the capacitors of C2 and C3 for the response improvement and the transient voltage drop reduction.

Table 3-B Recommended components for R1205xxxxA

|  | Rated voltage(V) | Part No. |
| :---: | :---: | :---: |
| C1 | 6.3 | CM105B105K06 |
| C2 | 50 | GRM31CR71H475M |
| C3 | 25 | $220 p F$ |
| R1 |  | For Vout Setting |
| R2 |  | For Vout Setting |
| R3 |  | $2 \mathrm{k} \Omega$ |

## R1205xxxxB/C

Set $0.22 \mu \mathrm{~F}$ or more capacitor C2 between Vout and GND pin. (R1205x8xxB) Set $0.47 \mu \mathrm{~F}$ or more capacitor C2 between Vout and GND pin. (R1205x8xxC) Note the Vout that depends on LED used, and select the rating of Vout or more.

Table 4 Recommended components for R1205xxxxB/C

|  | Rated voltage(V) | Part No. |
| :---: | :---: | :---: |
| C1 | 6.3 | CM105B105K06 |
| C2 | 25 | GRM21BR11E224 |
|  | 25 | C2012X7R1E474K |
|  | 50 | GRM21BR71H224 |

## External Components Setting

If the Vout spike noise is high, it may influence on the $\mathrm{V}_{\text {FB }}$ pin to cause the operation of $\mathrm{R} 1205 \times 8 \times x \mathrm{~A}$ unstable. To reduce the noise coming into $V_{F B}$ pin, please place a $1 \mathrm{k} \Omega$ to $5 \mathrm{k} \Omega$ resistor in $R 3$ in Fig. 1.

## Application of Using 5.5V or more Power Supply

Other than the IC power supply, if there is a power supply greater than 5.5 V , the high power output can be achieved by using the power supply as an inductor power supply. In this case, please place a capacitor between an inductor power supply and GND (shown in Fig. 2) aside from a bypass capacitor between the Vin pin and GND of the IC.


Fig. 1 R1205x8xxA


Fig . 2 R1205x8xxB/C

## The Method of Output Voltage Setting (R1205x8xxA)

The output voltage (Vоит) can be calculated with divider resistors (R1 and R2) values as the following formula:

$$
\text { Output Voltage }(\text { Vout })=V_{F B} \times(R 1+R 2) / R 1
$$

The total value of R1 and R2 should be equal or less than 300k . Make the $\mathrm{V}_{\mathrm{in}}$ and GND line sufficient. The large current flows through the $\mathrm{V}_{\mathrm{IN}}$ and GND line due to the switching. If this impedance ( $\mathrm{V}_{\mathrm{IN}}$ and GND line) is high, the internal voltage of the IC may shift by the switching current, and the operating may become unstable. Moreover, when the built-in Lx switch is turn OFF, the spike noise caused by the inductor may be generated.

## LED Current setting (R1205x8xxB/C)

When CE pin input is "H" (Duty=100\%), LED current can be set with feedback resistor (R1)

$$
l_{\text {LED }}=V_{\text {FB }} / R 1
$$

## LED Dimming Control (R1205x8xxB/C)

The LED brightness can be controlled by inputting the PWM signal to the CE pin. If the CE pin input is "L" in the fixed time (Typ. 0.5 ms ), the IC becomes the standby mode and turns OFF LEDs.
The current of LEDs can be controlled by Duty of the PWM signal of the input CE pin. The current of LEDs when High-Duty of the CE input is "Hduty" reaches the value as calculatable following formula.

$$
\text { ILed }=\text { Hduty } \times \mathrm{V}_{\mathrm{FB}} / \mathrm{R} 1
$$

The frequency of the PWM signal is using the range between 200 Hz to 300 kHz .
When controlling the LED brightness by the PWM signal of 5 kHz or less, $\mathrm{R} 1205 \times 8 \times x \mathrm{~B} / \mathrm{C}$ are recomended to avoide discharge function during dimming control.
When controlling the LED brightness by the PWM signal of 20 kHz or less, the increasing or decreasing of the inductor current might be make a sounds in the hearable sound wave area. In that case, please use the PWM signal in the high frequency area.


## ILed accuracy (R1205x8xxB / R1205x8xxC)

LED current (lled) is affected by the offset voltage of the error amplifier in the DC/DC converter.
LED might turn off due to the offset voltage variation, when brightness is controlled by low PWM duty cycle.
In case of R1205x8xxB, it is recommended to input PWM signal that has $18.5 \%$ or more duty.
In case of lower duty cycle than $18.5 \%$, it is recommended to use R1205x8xxC.
The table below shows the Iled accuracy of R1205x8xxC at low PWM duty cycle input (low brightness).

ILed accuracy when low PWM Duty is applied ( $\mathrm{R} 1=20 \Omega$ )

|  | PWM Duty applied to CE Pin | ILed Min. | Iled Max. |
| :---: | :---: | :---: | :---: |
| R1205x8xxC | $3.5 \%$ (Frequency $=20 \mathrm{kHz}$ to 300 kHz ) | $0.01 \mathrm{~mA}^{(1)}$ | $2.1 \mathrm{~mA}^{(1)}$ |

(1) Design guaranteed value $\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$

## TECHNICAL NOTES

## - Current Path on PCB

The current paths in an application circuit are shown in Fig. 3 and 4.
A current flows through the paths shown in Fig. 3 at the time of MOSFET-ON, and shown in Fig. 4 at the time of MOSFET-OFF. In the paths pointed with red arrows in Fig. 4, current flows just in MOSFET-ON period or just in MOSFET-OFF period. Parasitic impedance / inductance and the capacitance of these paths influence stability of the system and cause noise outbreak. So please minimize this side effect. In addition, please shorten the wiring of other current paths shown in Fig. 3 and 4 except for the paths of LED load.

## - Layout Guide for PCB

- Please shorten the wiring of the input capacitor (C1) between Vis pin and GND pin of IC. The GND pin should be connected to the strong GND plane.
- The area of $L x$ land pattern should be smaller.
- Please put output capacitor (C2) close to the Vout pin.
- Please make the GND side of output capacitor (C2) close to the GND pin of IC.


Fig. 3 MOSFET-ON


Fig. 4 MOSFET-OFF

- PCB Layout

PKG: DFN1616-6B pin
R1205LxxxA/xxxB/xxxC Typical Board Layout
Top Layer

- PKG:TSOT-23-6pin

R1205NxxxA/xxxB/xxxCTypical Board Layout


U1-
indicates the position of No. 1 pin.

## TYIPICAL CHARACTERISTICS

1) Efficiency vs. Output Current Characteristics (R1205N823A)


Vout=15V, L=10 $\mu \mathrm{H}$ (LQH32CN100K53)


Vout=20V, L=10 $\mu \mathrm{H}$ (LQH32CN100K53)


Vout=10V, L=22 $\mu \mathrm{H}$ (LQH32CN220K53)



Vout=20V, L=22 $\mu \mathrm{H}$ (LQH32CN220K53)



Typical Applications with Using 5.5V or Greater Vout=15V, L=10 $\mu \mathrm{H}$ (LQH32CN100K53)


Vout $=20 \mathrm{~V}, \mathrm{~L}=10 \mu \mathrm{H}$ (LQH32CN100K53)

2) Efficiency vs. Output Current Characteristics (R1205N823B/C)

4LED, L=10 $\mu \mathrm{H}$ (LQH32CN100K53)


4LED, L=22 $\mu \mathrm{H}$ (LQH32CN220K53)


5LED, L=10 $\mu \mathrm{H}$ (LQH32CN100K53)


6LED, L=10 $\mu \mathrm{H}$ (LQH32CN100K53)


5LED, L=22 $\mu \mathrm{H}$ (LQH32CN22OK53)


6LED, L=22 $\mu \mathrm{H}$ (LQH32CN220K53)


6LED, $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$


Typical Applications with Using 5.5V or Greater
$5 \mathrm{LED}, \operatorname{Vin}(\mathrm{IC})=3.6 \mathrm{~V}$

3) Output Voltage vs. Output Current (R1205N823A)

Vout=10V, L=10 $\mu \mathrm{H}$ (LQH32CN100K53)


Vout=15V, L=10 $\mu \mathrm{H}$ (LQH32CN100K53)

$6 \mathrm{LED}, \operatorname{Vin}(\mathrm{IC})=3.6 \mathrm{~V}$


V оит=10V, L=22 $\mu \mathrm{H}$ (LQH32CN220K53)


Vout=15V, L=22 $\mu \mathrm{H}$ (LQH32CN220K53)


$V_{\text {out }}=20 \mathrm{~V}, \mathrm{~V}_{\text {In }}=3.6 \mathrm{~V}$


Typical Applications with Using 5.5V or Greater VOUT=15V, L=10 $\mu \mathrm{H}$ (LQH32CN100K53)


Vout=20V, L=22 $\mu \mathrm{H}$ (LQH32CN220K53)


VOUT $=20 \mathrm{~V}, \mathrm{~L}=10 \mu \mathrm{H}$ (LQH32CN100K53)

4) Duty vs. ILED

R1205N823B/C

6) Waveform (6LED)


R1205N823B/C(CE Freq=300KHz)

5) OVP Output Waveform

R1205N823B/C


R1205N823B/C (CE Freq=10KHz)

7) Diode Forward Voltage vs. Temperature

8) Standby Current vs. Temperature

10) UVLO Output Voltage vs. Temperature

R1205x8xxA


## 9) Supply Current vs. Temperature



11) VFB Voltage vs. Temperature

12) Switch ON Resistance RON vs. Temperature


R1205x8xxB

13) OVP Voltage vs. Temperature

14) LX Current Limit vs. Temperature

15) Oscillator Frequency vs. Temperature


R1205x82xx

16) Maxduty vs. Temperature

17) Thermal Shutdown Detect / Release Temperature vs. Input Voltage


## 18) Load Transient Response

$\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {OUT }}=15 \mathrm{~V}$ lout $=0 \mathrm{~mA} \Leftrightarrow 30 \mathrm{~mA}$
$\mathrm{L}=10 \mu \mathrm{H}$ Setting : Table 3-A

$\mathrm{L}=22 \mu \mathrm{H} \quad$ Setting : Table 3-A

$\mathrm{L}=10 \mu \mathrm{H} \quad$ Setting : Table 3-B



$\mathrm{L}=22 \mu \mathrm{H} \quad$ Setting : Table 3-B


The power dissipation of the package is dependent on PCB material, layout, and environmental conditions. The following measurement conditions are based on JEDEC STD. 51.

Measurement Conditions

| Item | Measurement Conditions |
| :--- | :--- |
| Environment | Mounting on Board (Wind Velocity $=0 \mathrm{~m} / \mathrm{s}$ ) |
| Board Material | Glass Cloth Epoxy Plastic (Four-Layer Board) |
| Board Dimensions | $76.2 \mathrm{~mm} \times 114.3 \mathrm{~mm} \times 0.8 \mathrm{~mm}$ |
| Copper Ratio | Outer Layer (First Layer): Less than $95 \%$ of 50 mm Square <br> Inner Layers (Second and Third Layers): Approx. $100 \%$ of 50 mm Square <br> Outer Layer (Fourth Layer): Approx. $100 \%$ of 50 mm Square |
| Through-holes | $\phi 0.2 \mathrm{~mm} \times 25$ pcs |

Measurement Result
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{Tjmax}=125^{\circ} \mathrm{C}\right)$

| Item | Measurement Result |
| :--- | :---: |
| Power Dissipation | 2400 mW |
| Thermal Resistance (日ja) | $\theta \mathrm{ja}=41^{\circ} \mathrm{C} / \mathrm{W}$ |
| Thermal Characterization Parameter ( $\psi \mathrm{j} \mathrm{t})$ | $\psi j \mathrm{j}=11^{\circ} \mathrm{C} / \mathrm{W}$ |

Өja: Junction-to-Ambient Thermal Resistance
$\psi j$ t: Junction-to-Top Thermal Characterization Parameter


Power Dissipation vs. Ambient Temperature


Measurement Board Pattern


DFN1616-6B Package Dimensions (Unit: mm)

[^0]Nisshinbo Micro Devices Inc.

The power dissipation of the package is dependent on PCB material, layout, and environmental conditions. The following conditions are used in this measurement.

Measurement Conditions

|  | Standard Test Land Pattern |
| :---: | :---: |
| Environment | Mounting on Board (Wind Velocity $=0 \mathrm{~m} / \mathrm{s}$ ) |
| Board Material | Glass Cloth Epoxy Plastic (Double-Sided Board) |
| Board Dimensions | $40 \mathrm{~mm} \times 40 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ |
| Copper Ratio | Top Side: Approx. $50 \%$ |
| Bottom Side: Approx. $50 \%$ |  |
| Through-holes | $\phi 0.5 \mathrm{~mm} \times 44 \mathrm{pcs}$ |

Measurement Result $\quad\left(\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{Tjmax}=125^{\circ} \mathrm{C}\right)$

|  | Standard Test Land Pattern |
| :---: | :---: |
| Power Dissipation | 460 mW |
| Thermal Resistance | $\theta \mathrm{ja}=\left(125-25^{\circ} \mathrm{C}\right) / 0.46 \mathrm{~W}=217^{\circ} \mathrm{C} / \mathrm{W}$ |
|  | $\theta \mathrm{jc}=40^{\circ} \mathrm{C} / \mathrm{W}$ |



Power Dissipation vs. Ambient Temperature


IC Mount Area (mm)

Measurement Board Pattern


TSOT-23-6 Package Dimensions (Unit: mm)

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Nisshinbo Micro Devices Inc.

## Official website

https://www.nisshinbo-microdevices.co.jp/en/

## Purchase information

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[^0]:    * The tab on the bottom of the package shown by blue circle is a substrate potential (GND). It is recommended that this tab be connected to the ground plane pin on the board but it is possible to leave the tab floating.

